



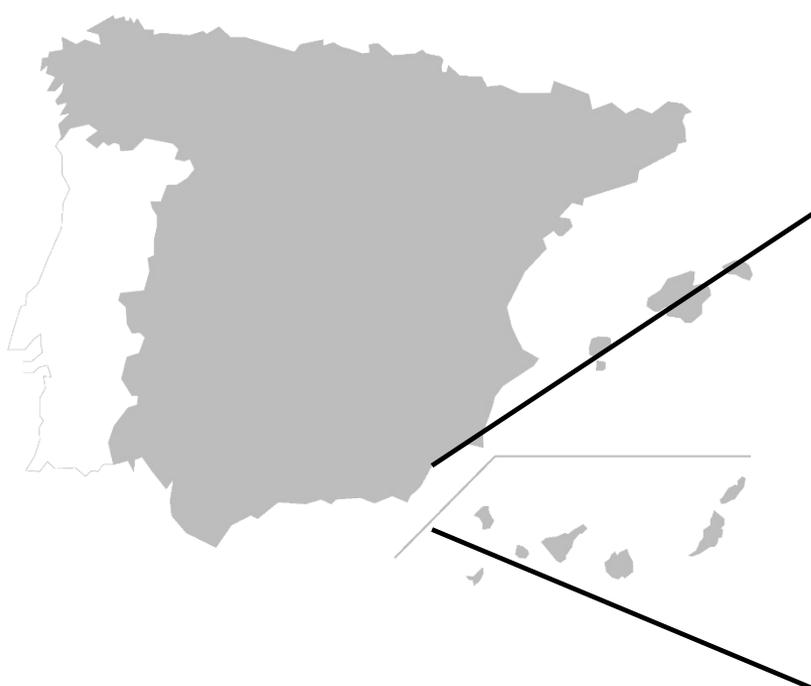
Shadowing and blocking effect optimization for a variable geometry heliostat field

Pablo Cádiz, Miguel Frasset, Manuel Silva,
Fernando Martínez, Jose Carballo



CTAER (Centro Tecnológico Avanzado de Energías Renovables)

Advanced Technology Centre for Renewable Energies

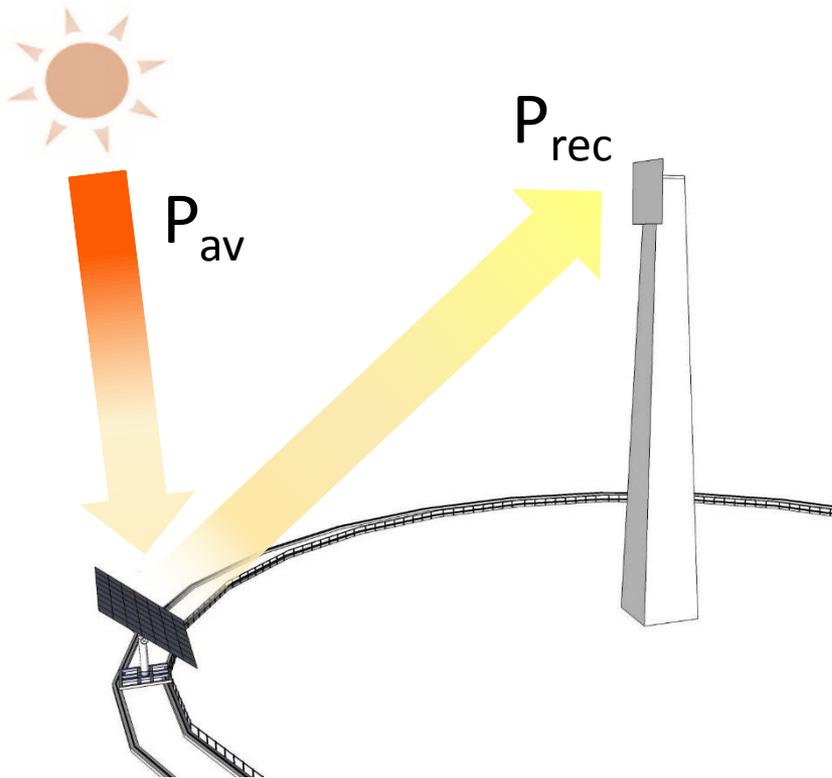


R&D

-  Biomass (*Menjibar-Jaen*)
-  Marine (*Tarifa-Cádiz*)
-  CSP (*Tabernas-Almería*)



- Area: 91 ha
- Multidisciplinary:
 - **PTC**
 - **CRS**
 - **H₂ & CPV**
 - **L/M Temp**
 - **Offices/Labs**



Optical efficiency (η_{opt})

Available power

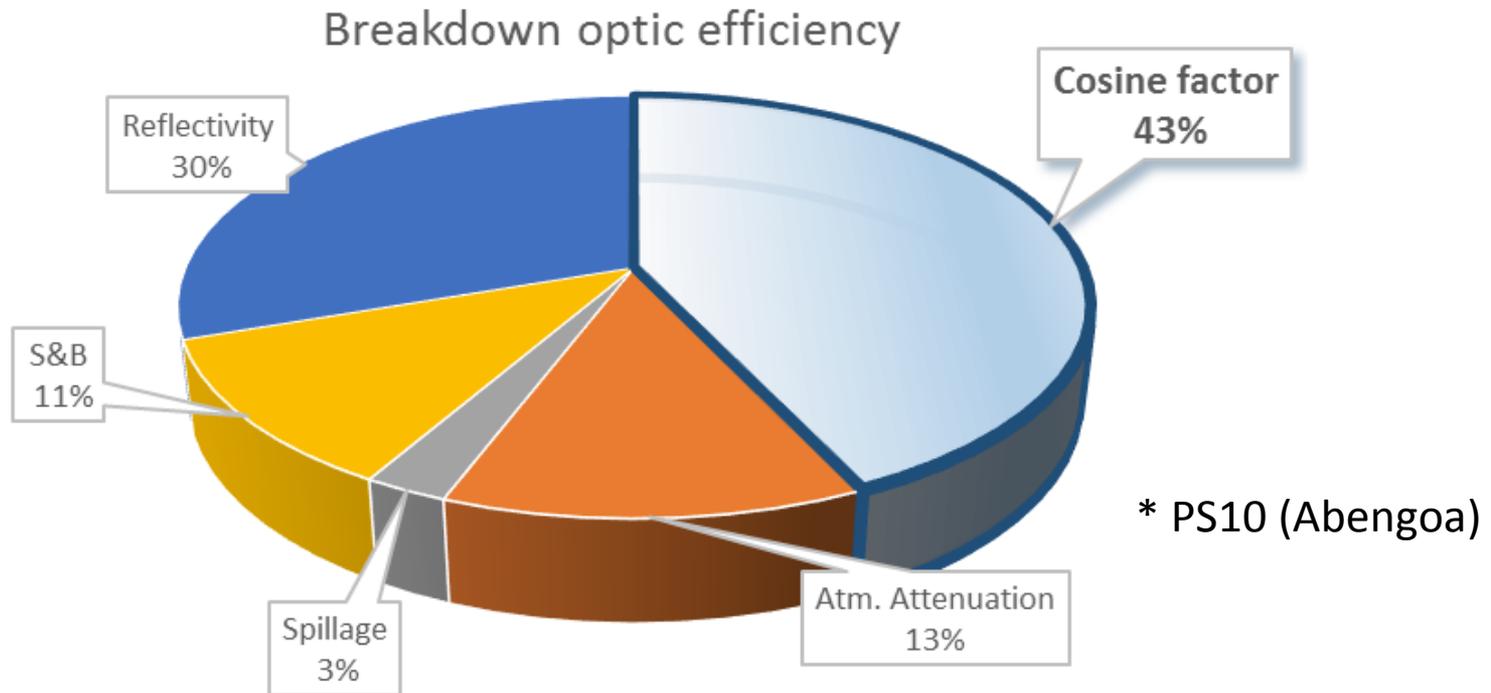
$$P_{av} = DNI \cdot A_{ap}$$

Power at the receiver

$$P_{rec}$$

$$\eta_{opt} = \frac{P_{REC}}{P_{av}}$$

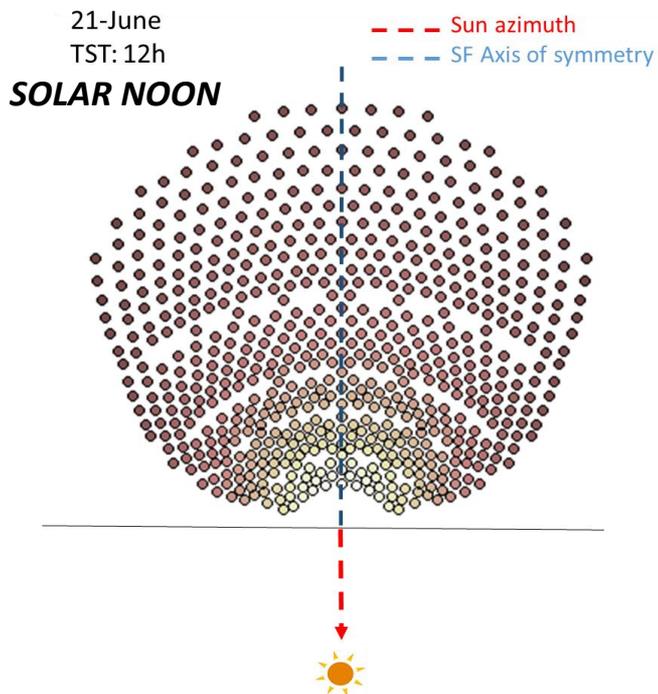
$$\eta_{opt}(x, y, t) = \rho \cdot f_{\cos\theta}(x, y, t) \cdot f_{at}(x, y) \cdot f_{spill}(x, y, t) \cdot f_{sb}(x, y, t)$$



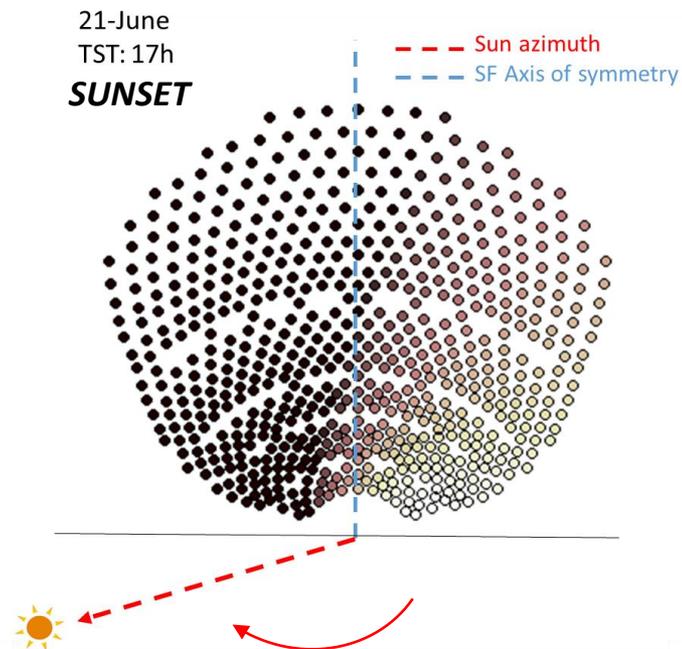
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IMPROVING THE COSINE FACTOR

CASE 1 --> $f_{\cos} = 0.87$

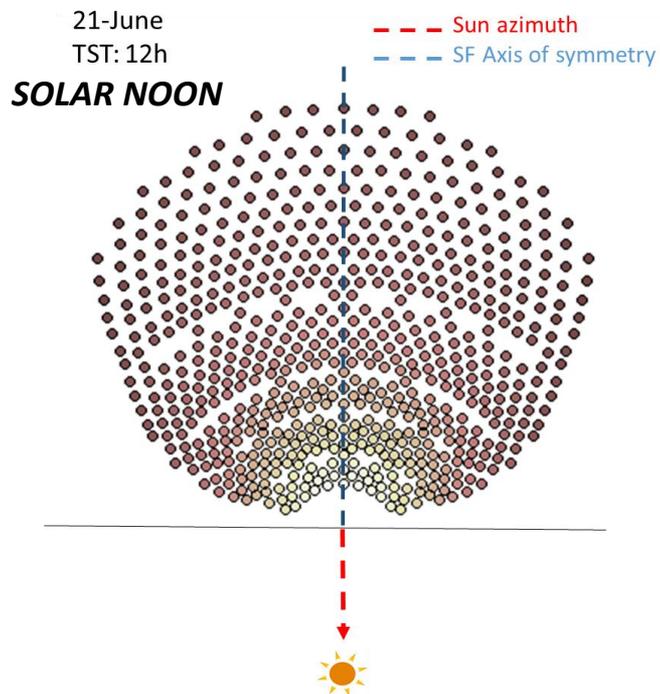


CASE 2 --> $f_{\cos} = 0.80$



IMPROVING THE COSINE FACTOR

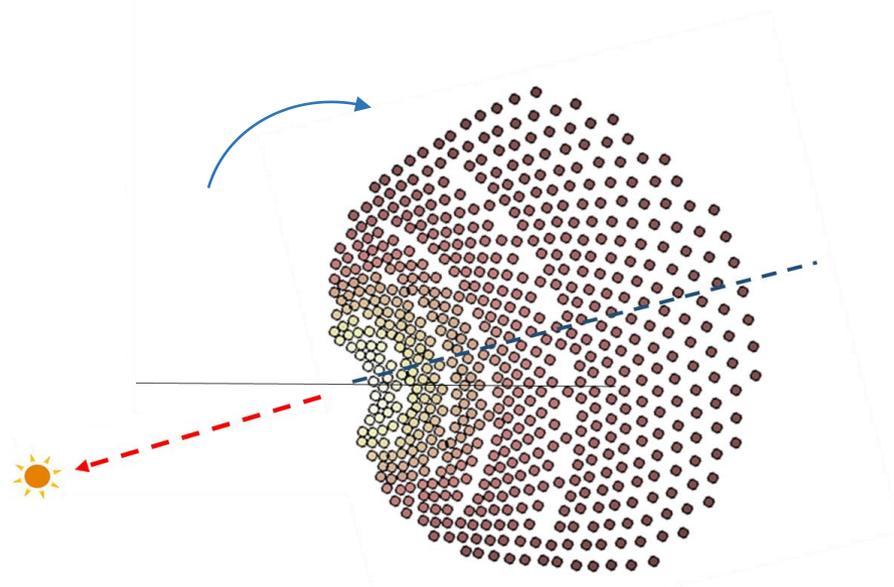
CASE 1 --> $f_{\text{cos}} = 0.87$

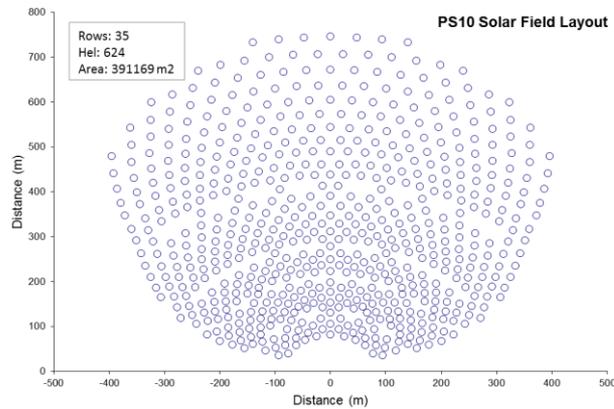


CASE 2 --> $f_{\text{cos}} = 0.80$

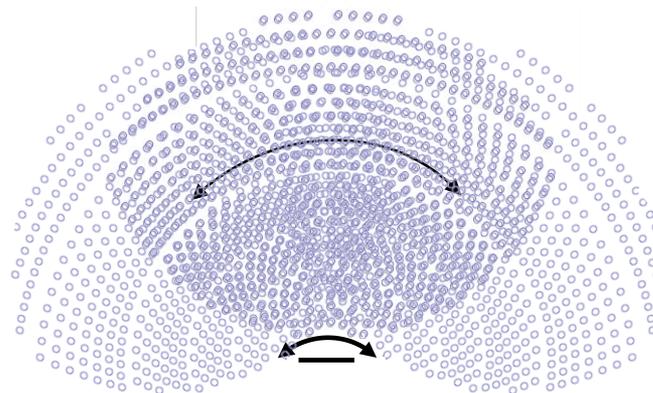
CASE 2a --> $f_{\text{cos}} = 0.88$

21-June
TST: 17h
SUNSET





CONVENTIONAL STAGGERED FIELD



VARIABLE GEOMETRY STAGGERED FIELD



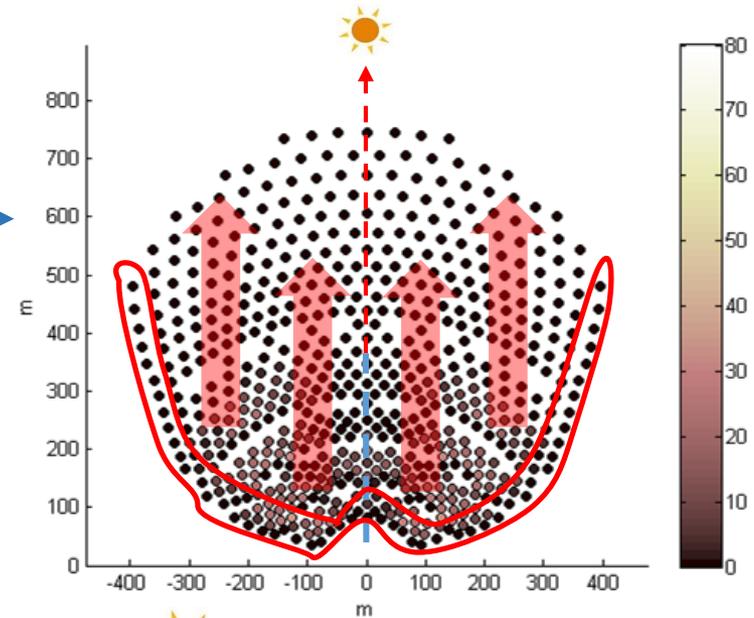
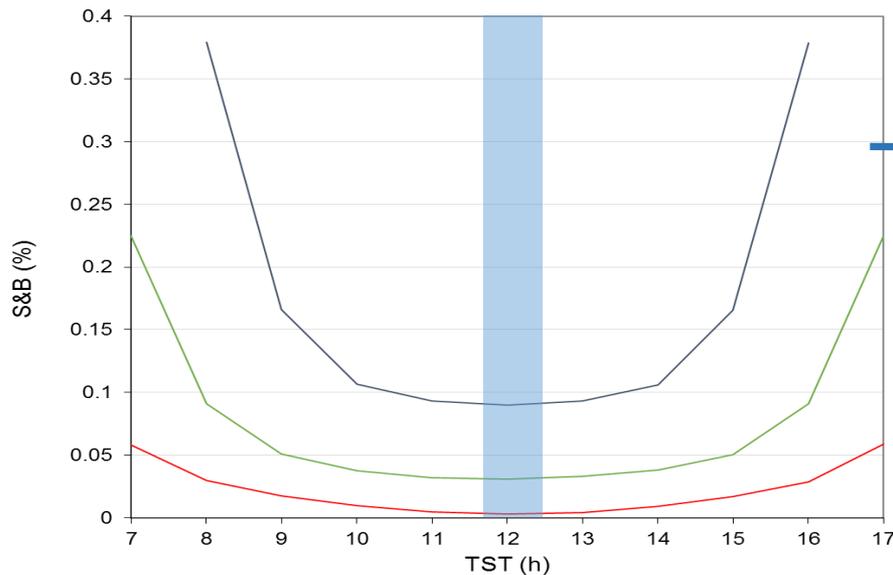
Mobile heliostats



Concentric circular rails

$$\eta_{opt}(x, y, t) = \rho \cdot f_{\cos\theta}(x, y, t) \cdot f_{at}(x, y) \cdot f_{spill}(x, y, t) \cdot f_{sb}(x, y, t)$$

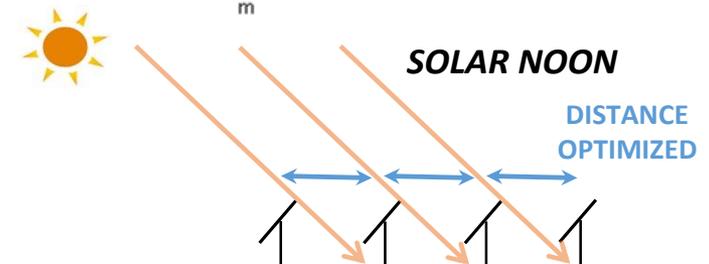
Shadowing & Blocking losses



Winter solstice

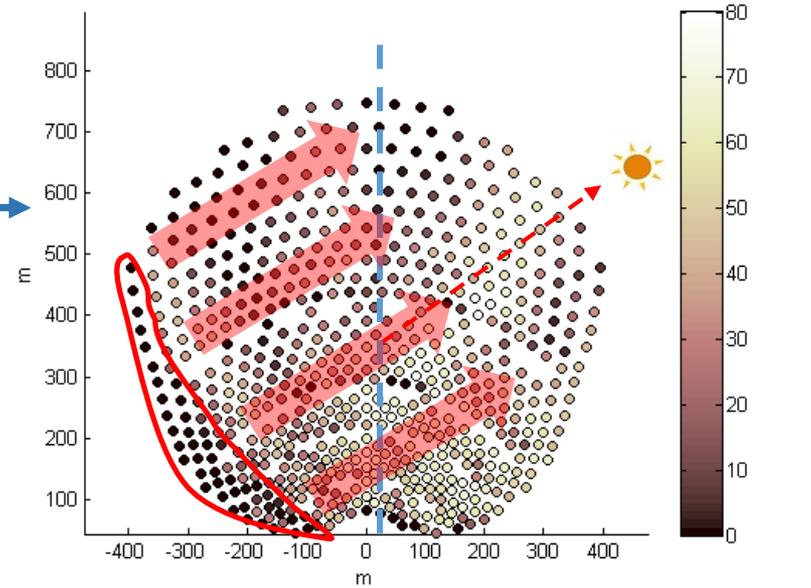
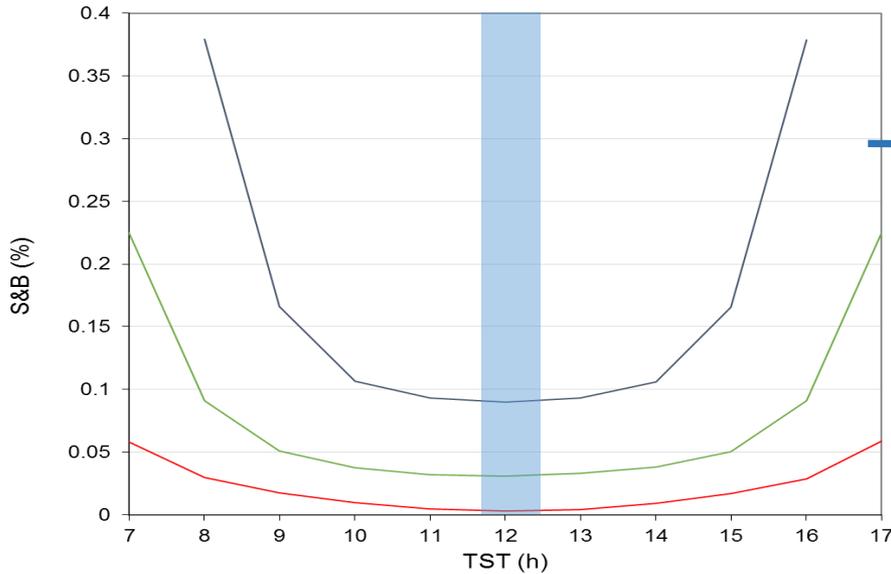
Equinox

Summer solstice



$$\eta_{opt}(x, y, t) = \rho \cdot f_{\cos\theta}(x, y, t) \cdot f_{at}(x, y) \cdot f_{spill}(x, y, t) \cdot f_{sb}(x, y, t)$$

Shadowing & Blocking losses



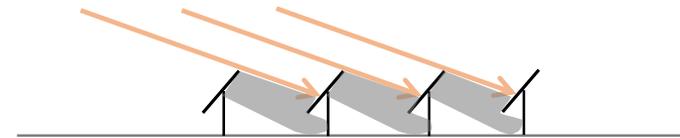
Winter solstice

Equinox

Summer solstice

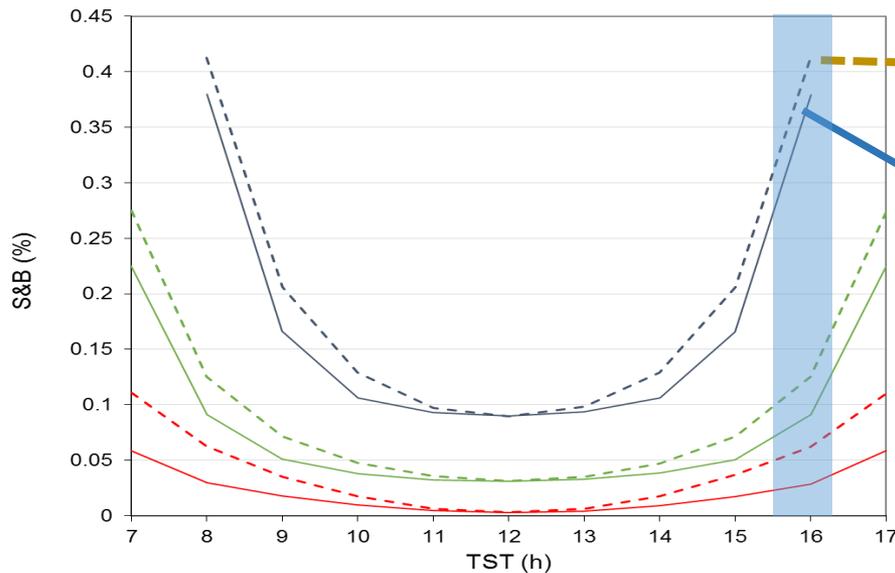


SUNSET



$$\eta_{opt}(x, y, t) = \rho \cdot f_{\cos\theta}(x, y, t) \cdot f_{at}(x, y) \cdot f_{spill}(x, y, t) \cdot f_{sb}(x, y, t)$$

Shadowing & Blocking losses

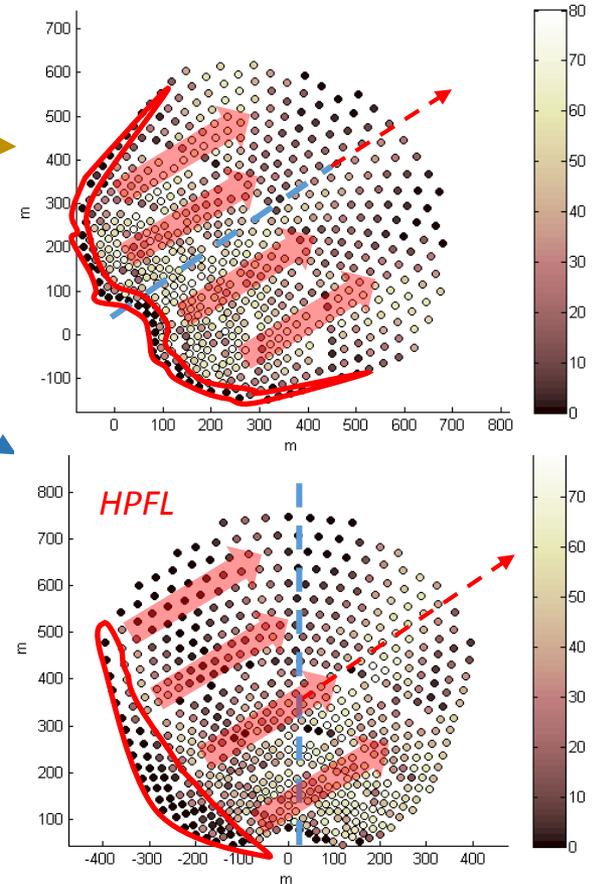


ANNUAL LOSSES (1 - f _{sb})	
NORTH FIELD	7%
ROTATING FIELD	8.7%

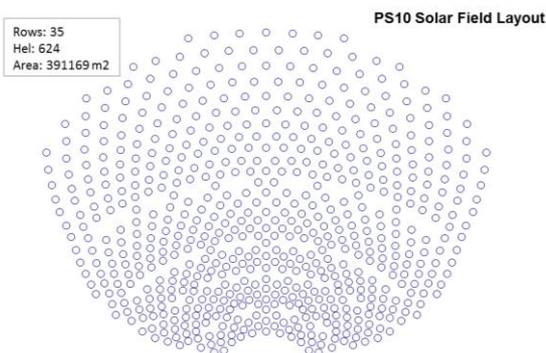
Winter solstice

Equinox

Summer solstice



Stationary Field

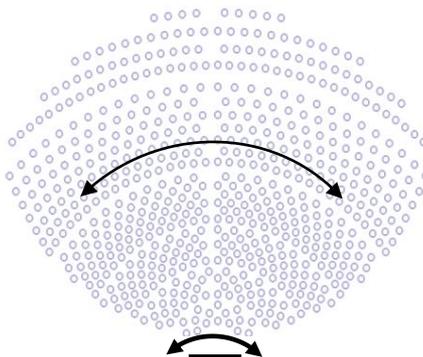


LAYOUT OPTIMIZATION

21 variables
(radial distance, azimuthal distance, incremental spacing between rows...)

Commercial codes

Variable Geometry Field Common Operation strategy

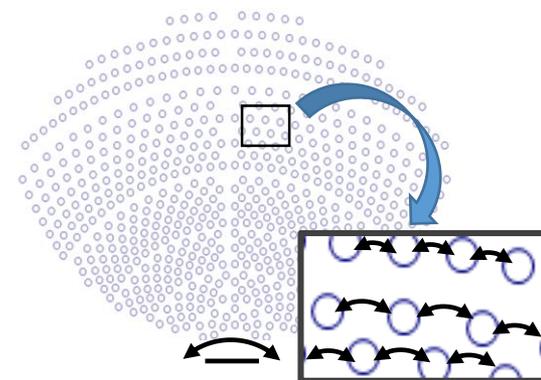


LAYOUT OPTIMIZATION

18 variables
(radial distance, azimuthal distance, incremental spacing between rows...)
+
Field Velocity

Modification over existing codes

Variable Geometry Field Individual Operation strategy



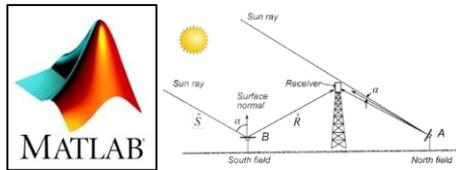
LAYOUT OPTIMIZATION

624 variables
(Heliostat position)
+
Field Velocity

NEW CODE

CODE STRUCTURE

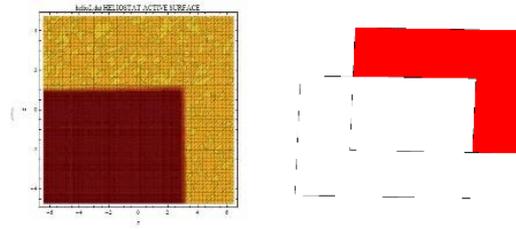
New code developed in MatLab (Energy simulation)



Optimization problem

Heliostat position with field symmetry
 $\text{Int}(n/2)$
 +
 Field Velocity

Re-design Shadow & Blocking calculation engine



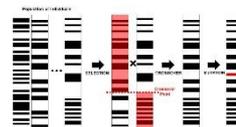
Validation



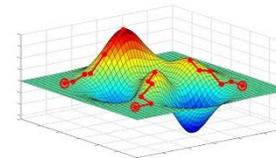
On field real validation

Ray-tracing
 Commercial codes

Optimization algorithm



Genetic algorithm



Modified deterministic hill-climbing

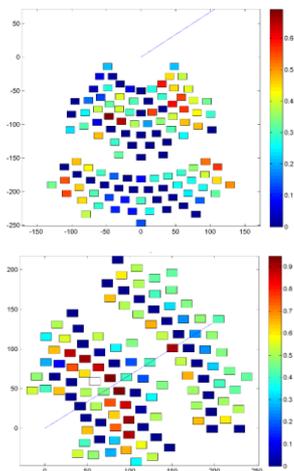


Validation

NSPOC

(Hourly Energy simulations)

RESULTS (4pm – 113hel)



FIELD	Cosine effect efficiency (CE)	Shadowing effect efficiency (SE)	Combined effect (CE*SE)
STATIONARY STAGGERED			
ROTATING STAGGERED COMMON OPERATION			
ROTATING INDIVIDUAL OPERATION			

SIMULATION TIME

8.3 min

2 weeks

- Although rotating fields show significant benefits in terms of optical efficiency, rotating the whole field keeping the staggered structure decreases the Shadowing & Blocking performance
- It is necessary to use an individual operation strategy instead of a common strategy
- To calculate the heliostat position in each moment is necessary to solve an optimization problem of a significant number of variables
- The code developed by CTAER reduces the time spent in S&B calculations and uses new optimization algorithms
- Using an individual control strategy the combined effect of the cosine factor and S&B can be improved more than 10% with respect to a north stationary field.

Thanks for your attention!



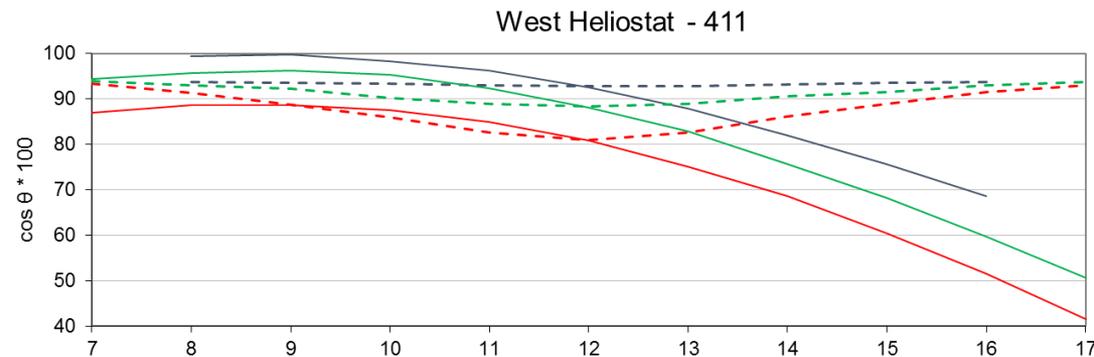
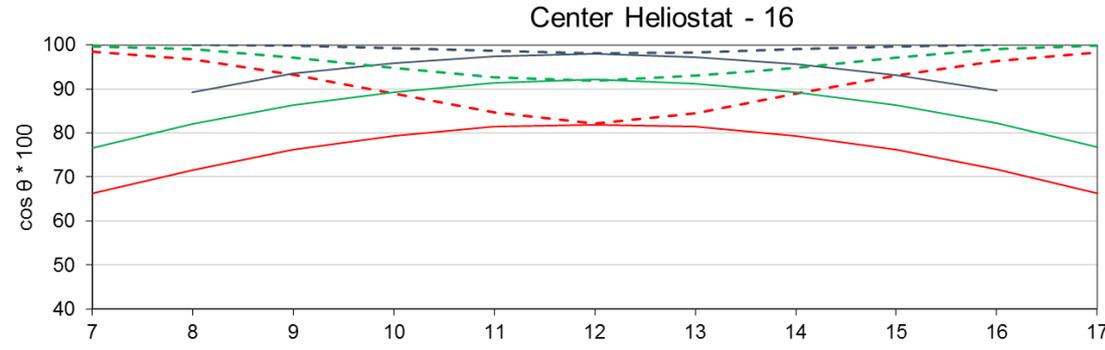
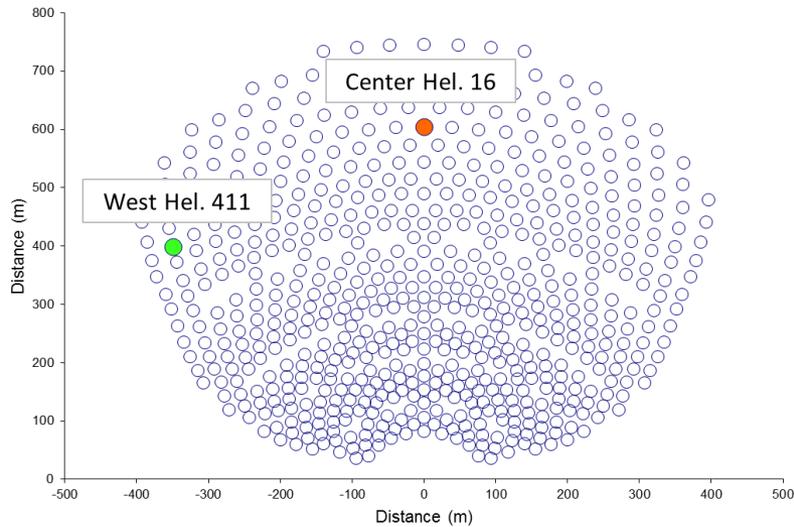
For further information please contact:

- Miguel Frasset Herraiz miguel.frasquet@ctaer.com
- Sol Luca de Tena sol.lucadetena@ctaer.com

APPENDIX

$$\eta_{opt}(x, y, t) = \rho \cdot \underline{f_{\cos\theta}(x, y, t)} \cdot f_{at}(x, y) \cdot f_{spill}(x, y, t) \cdot f_{sb}(x, y, t)$$

Cosine factor



ANNUAL LOSSES (1 - $f_{\cos\theta}$)	
NORTH FIELD	12.6%
ROTATING FIELD	6%

— NF
- - - RF
Winter solstice Equinox Summer solstice

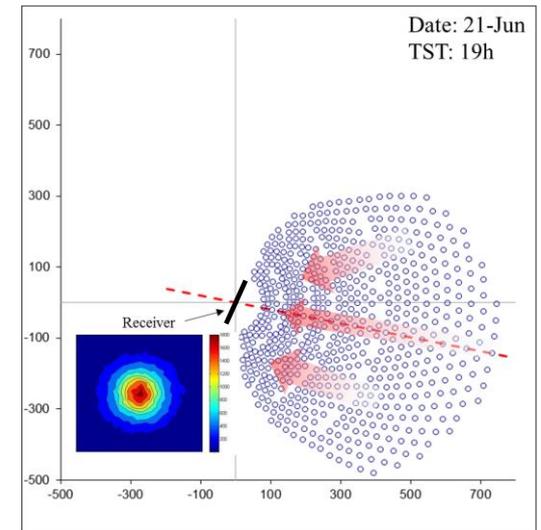
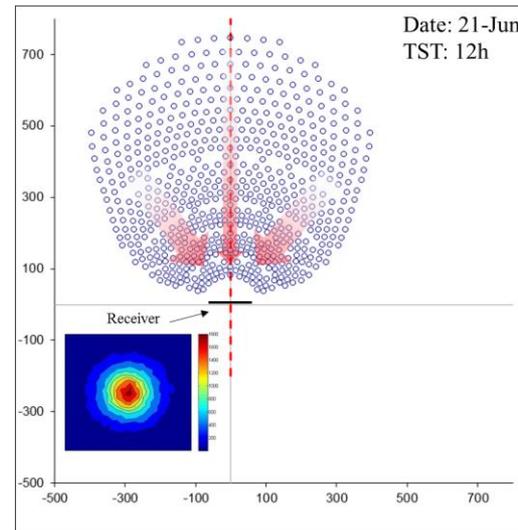
$$\eta_{opt}(x, y, t) = \cancel{\rho} \cdot f_{\cos\theta}(x, y, t) \cdot \cancel{f_{at}(x, y)} \cdot \underline{f_{spill}(x, y, t)} \cdot f_{sb}(x, y, t)$$

Spillage

- ~~Size of the receiver~~
- ~~Slant range~~
- ~~Incidence angle on the receiver~~
- Optic aberration (Astigmatism)

CASE 1 = CASE 2

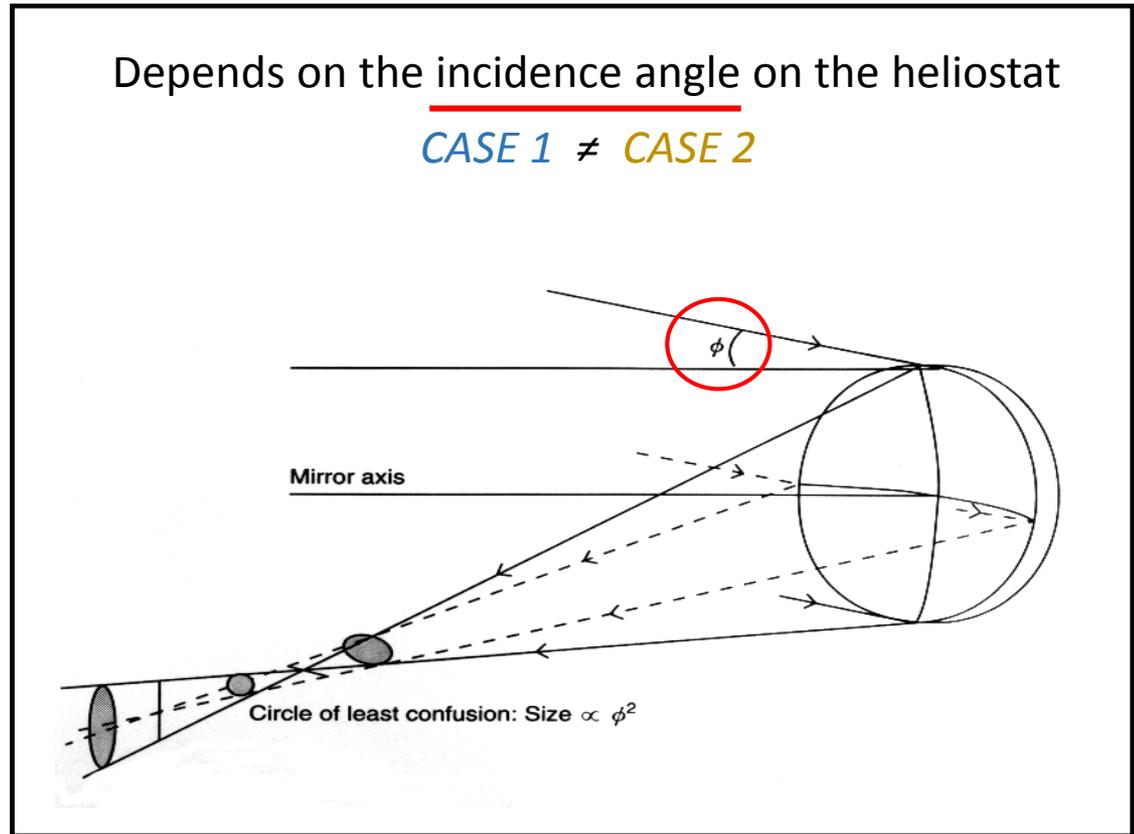
Same Incidence angle on the receiver in both cases



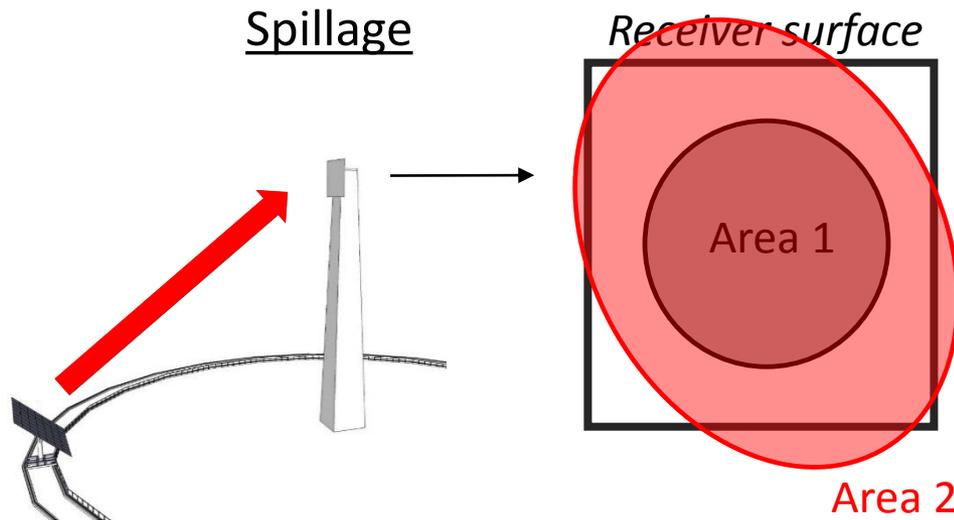
$$\eta_{opt}(x, y, t) = \cancel{\rho} \cdot f_{\cos\theta}(x, y, t) \cdot \cancel{f_{at}(x, y)} \cdot \underline{f_{spill}(x, y, t)} \cdot f_{sb}(x, y, t)$$

Spillage

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$$\eta_{opt}(x, y, t) = \cancel{\rho} \cdot f_{\cos\theta}(x, y, t) \cdot \cancel{f_{at}(x, y)} \cdot \underline{f_{spill}(x, y, t)} \cdot f_{sb}(x, y, t)$$



Reflected image	Incidence angle	Area
<i>Ideal</i>	= 0	Area 1

$$\left(\frac{h_s}{\beta_s \cdot d} \right) = \frac{\text{Area 2}}{\text{Area 1}}$$

Represents the increase of the reflected image with respect to the ideal one (incident angle equal to zero)

Dimensionless
size